

## **Síntesis de geopolímeros a partir de la activación alcalina de residuos de minería del oro**

## **Synthesis of geopolymers from alkaline activation of gold mining wastes**

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### **Resumen**

Este trabajo presenta los resultados preliminares relacionados con el desarrollo de polímeros inorgánicos (geopolímeros) a partir de la activación alcalina de residuos de la minería de oro. La caracterización mineralógica y fisicoquímica de estos residuos de minería de oro muestra su gran potencial como fuente de precursores geopoliméricos como una alternativa razonable para el desarrollo de aglutinantes activados alcalinamente amigables con el medio ambiente. El proceso de geopolimerización es un camino viable para transformar estos residuos en materiales con alta resistencia mecánica, alta inercia química y alta durabilidad en el tiempo, dando valor agregado a los subproductos de la actividad minera.

**Palabras clave:** *Activación alcalina, geología ambiental, geopolímeros, subproductos mineros.*

### **Abstract**

This paper reports preliminary results related to the development of inorganic polymers (geopolymers) from alkali-activation of gold mining wastes. Mineralogical and physicochemical characterization of these gold mining wastes shows their significant potential as geopolymeric source precursors as a reasonable alternative to the development of alkali-activated friendly environmental binders. Geopolymerization process is a viable way to transform these residues in materials with high mechanical strength, high chemical inertness and high durability over time, giving add value to the by-products of the mining industry.

**Keywords:** *Alkaline activation, environmental geology, geopolymers, mining products.*

## 1. Introduction

The demand for Portland cement as a worldwide construction material increases as a result of population growth and economic development. By 2011, the global annual production of cement was about 3.4 million tonnes (USGS, 2012). However, its production generates the emission of toxic gases ( $\text{CO}_2$ ,  $\text{SO}_2$  y  $\text{NO}_x$ ) (Gartner, 2004). However, the cement industry is responsible to 5-7% of anthropogenic global  $\text{CO}_2$  emissions (Barcelo and Kline, 2012).  $\text{CO}_2$  emissions are associated with decarbonization of limestone in the furnace of clinkerization (Puertas *et al.*, 2006). The production of one tonne of Portland cement generates 0.55 tonnes of chemical  $\text{CO}_2$  and requires an additional 0.39 tonnes of  $\text{CO}_2$  in fuel emissions for baking and grinding, accounting for a total of 0.94 tonnes of  $\text{CO}_2$  (Gartner, 2004). It is known that the cement industry promotes the use of alternative materials contributing to the sustainable development with low  $\text{CO}_2$  emissions and proper use of natural resources, mainly due to the remarkable concern for environmental problems arising from global warming. To try to mitigate the issue of the huge amount of this type of gas, the cement industry has opted for the use of a number of additives.

The synthesis of geopolymers has resorted to the use of various industrial wastes, such as slag crystallized furnace volcanic ash (Sanjayan and Sioulas, 2000; Cheng and Chiu, 2003), fly ash (Swanepoel and Strydom, 2002; Bakharev, 2005; Fernández-Jiménez and Palomo, 2005; Temuujin *et al.*, 2013), incinerator ash (Shih and Yokohama, 2003; Lancellotti *et al.*, 2010; Luna-Galiano *et al.*, 2011), aluminum recycling waste (Puertas *et al.*, 1999; van Riessen *et al.*, 2013), paper sludge and paper sludge ash (Hauser *et al.*, 1999), ceramic wastes (Puertas *et al.*, 2006) and mining wastes (Singh and Garg, 2000; Pacheco-Torgal *et al.*, 2008; Soares *et al.*, 2008; Caballero and Sánchez, 2010; Zhang *et al.*, 2011) as alternative materials in the manufacture of geopolymers, which has become a very effective way to reach, a large extent, this sustainable development. Notwithstanding this, many efforts are still being made to find new

materials that can be used in the manufacturing process and production of cementitious products; the synthesis of geopolymers from mining waste turns out to be a good alternative as a long-term solution. In terms of global warming, the preparation of cementitious materials based geopolymers helps reduce  $\text{CO}$  emissions, without economic sacrifices for the industry, such that there is a total use of all materials and resources used in mining.

Pacheco-Torgal *et al.* (2007; 2008) show that it is possible to obtain a cementitious geopolymeric material from the muddy tailings of the Panasqueira tungsten mine (Portugal), proving that these wastes had a high content of muscovite and quartz, which in chemical terms means that they correspond alumina- and silica-rich materials. Based on the fact that geopolymerization processes can be result in aluminium silicate materials under highly alkaline conditions (Davidovits, 1994), the feasibility of using these residues in the synthesis of a friendly cementitious geopolymeric material of low cost long-term and very high mechanical and chemical resistance was demonstrated.

This work is focused on evaluating the performance of cementitious materials based on inorganic polymers (geopolymers), obtained from the use of gold mining by-products. The chemical and mineralogical characterization of the mining wastes of interest in this study determines their possible use as an alternative raw material for preparing geopolymer-based mortars. The main contribution of this research to generate new knowledge refers to the mitigation of the environmental impact by transforming gold mining by-products in geopolymers for use as building materials.

## 2. Materials and experimental procedure

### 2.1 Raw materials

Type I Portland cement was used in this study as reference cement. It is manufactured by Holcim S.A. (Colombia), Nobsa (Boyacá). The raw material used as an additive in the preparation of

geopolymer mortars corresponds to gold mine tailings from the La Baja Mine, which results after the process of grinding and separation of sulfides from quartz feldspathic gneisses exhibiting silicification. It was sun-dried for 3 days, then it was pulverized in a RETSCH Mortar Grinder RM 100 and sieved in order to use a particle size less than 62.5 microns for the preparation of the geopolymeric mortars. The sand used in the preparation of the different mixtures was extracted from the Chicamocha River (Santander). It was sun-dried for 3 days and sieved in order to use a uniform grain size. The gold mining wastes were activated with sodium hydroxide (NaOH) in pellets of 98% purity and neutral sodium silicate (NaSiO<sub>3</sub>) 42 with molar ratio of SiO<sub>2</sub>:Na<sub>2</sub>O ≈ 3.0, which were commercially purchased from CONQUIMICA.

## 2.2 Characterization of the raw materials

The fineness of any cementing material affects its rate of hydration. Thus, the finer the material, the greater its rapidity of hydration, and, therefore, the greater the development of mechanical strength, as established by the test standard NTC 226 (ICONTEC, 1998). To carry out the determination of the fineness of the starting material, 100 g of sample were sieved through 200-mesh standard sieve. Then, the material that could pass through the mesh was removed from the bottom and weighed. The calculations were obtained from the following equation:

$$F = 100 - R_c$$

Where,  $F$  = fineness y  $R_c$  = corrected residue

To define  $R_c$ , the following equation was used:

$$R_c = \frac{R_s}{(100 + C)}$$

Where,  $R_s$  = retained residue in the 200-mesh and  $C$  = sieve correction factor

In our case, the sieve correction factor ( $C$ ) was zero, while the value of the corrected residue

was 0.65 g. Replacing these values in each of the expressions above, it was determined that the fineness of the gold mining waste is 99.35%, a value very well accepted from the textural point of view, considering that the same procedure was performed on the type I Portland cement, which shows a fineness of 99.11%.

The particle size analysis of the aggregate was conducted using the test standard E-123 INV (INVIAS, 2007), initially determining the weight of the granular fraction and separating the particles in different sizes (1.180, 0.600, 0.425, 0.250 and 0.150 mm) using sieves in decreasing order. Finally the weight of each retained fraction was determined by verifying that the sum of the weight retained on each sieve is equal to the initial weight of the granular fraction, with a tolerance of 0.5%.

The characterization of the raw materials was performed using different analytical techniques, which are described below. The chemical composition of the raw materials was investigated using a EDX-800HSEnergy Dispersive X-ray Fluorescence Spectrometer, which has a Si(Li) solid state detector, rhodium X-ray tube, and 10 mm collimator without filter. The quantification of the elements was performed using the method of fundamental parameters (FP) using the software DXP-700E version 1.00 Rel. 014. Mineral phases were studied by X-ray powder diffraction (XRPD) using a Rigaku D/MAX IIIB powder diffractometer working in Bragg-Brentano geometry and equipped with a NaI(Tl) scintillation detector. A Cu-K $\alpha$ , radiation ( $\lambda = 1.5406 \text{ \AA}$ ), a graphite monochromator, a fixed Soller slit, a divergence slit of 1° and a 0.3-mm receiving slit were used. The diffractometer was operated over the range 2-70° ( $2\theta$ ) at 40 kV and 30 mA, using step scan with a step size of 0.02°  $2\theta$ . Phase identification was performed using the crystallographic database Powder Diffraction File (PDF-2) from International Centre for Diffraction Data (ICDD). Full-pattern Rietveld refinement using RIQAS 3.1 program (MDI Inc.) was performed to quantify the amounts (wt%) of phases. The raw materials were also examined by Fourier transformed infrared (FTIR) spectroscopy

by using a Bruker FTIR Tensor 27 Spectrometer. The spectra were obtained in the 400-4000 cm<sup>-1</sup> region. Approximately 2 mg of the sample plus 200 mg of KBr were weighted out, milled and grounded in a mortar. The resulting mixture was then pressed into a pellet.

### 2.3 Synthesis of geopolymers

In the synthesis of geopolymers, the standard test NTC 220 (ICONTEC, 1998) was followed. This standard states that for preparing 6 cement mortars, using molds of 50 mm side, the mass fractions must be composed by 1 part of the cementitious material and 2.75 parts of the aggregate (sand). On the other hand, the ratio of water solution/cementitious material should be 0.48. Several percentages of the starting material (50%, 70%, 80%, 90%) were added to the conventional cement in the synthesis process. In order to differentiate each of the resultant

geopolymer, the code GEW-%-8/16 was used, where the prefix GEW corresponds to the initials of the geopolymer and the names of the two main authors of this research paper; % is the proportion between the starting material and the type I Portland cement; 8/16 is the concentration of the NaOH solution used in the alkaline activation process. Therefore, the geopolymer GEW-50-8 corresponds to a synthesized material from a mixture of 50% of type I Portland cement + 50% of alkaline activated mining waste in a NaOH (8M) + Na<sub>2</sub>SiO<sub>3</sub> (16M) solution. The relationship used in the activating solution NaOH:Na<sub>2</sub>SiO<sub>3</sub> was 1:2. Taking into account the NTC 220 standard, the experimental parameters for the preparation of geopolymers are summarized in Table 1.

### 2.4 Technological tests

The mechanical behavior of the synthesized material was measured by conducting

Table 1. Quantification of the materials according to the NTC 220 standard.

GMW (g)	CPO (g)	GMW/CPO ratio	A (g)	NaOH 8M (ml)	Na <sub>2</sub> SiO <sub>3</sub> 8M (ml)	Activating solution/GMW+CPO+A
1 part			2.75 parts			0.485 parts
250	250	2.75	1375	81	161	
350	150	2.75	1375	81	161	
400	100	2.75	1375	81	161	Test
450	50	2.75	1375	81	161	
Compressive strength (7, 14 and 28 days)						
Attack with H <sub>2</sub> SO <sub>4</sub> (4 weeks)						
Attack with MgSO <sub>4</sub> (4 weeks)						
High temperatures						
GMW (g)	CPO (g)	GMW/CPO ratio	A (g)	NaOH 16M (ml)	Na <sub>2</sub> SiO <sub>3</sub> 8M (ml)	Relación solución activante / GMW+CPO+A
1 parte			2.75 partes			0.485 parts
250	250	2.75	1375	81	161	
350	150	2.75	1375	81	161	
400	100	2.75	1375	81	161	Test
450	50	2.75	1375	81	161	
Compressive strength (7, 14 and 28 days)						
Attack with H <sub>2</sub> SO <sub>4</sub> (4 weeks)						
Attack with MgSO <sub>4</sub> (4 weeks)						
High temperatures						

GMW, gold mining waste; CPO, ordinary Portland cement; A, aggregate; activating solution, NaOH+Na<sub>2</sub>SiO<sub>3</sub> in relation 1:2.5.

compressive strength tests, whereas their performance and durability was evaluated under extreme conditions (attack by acids and sulfates, and high temperatures). In each test, the performance and durability of each geopolymer was compared with mortars made with type I cement Portland. Four mortars in each of the tests were used. This was done in order to be able to draw a representative average value. 672 mortars were prepared.

#### 2.4.1 Compressive strength tests

These tests were conducted leaving each geopolymer to different storage times according to the account the NTC 220 standard. A polyethylene film completely isolated each of the specimens during curing times of 7, 14, 21, and 28 days. At each of these times a total of 4 mortars were used in order to get a representative average of the test. These tests were conducted using a Shenck Trebel universal testing machine.

#### 2.4.2 Compressive strength tests under extreme conditions of acidity, salinity and high temperatures

These tests intended to simulate a scenario where geopolymers were exposed to extreme conditions of acidity, salinity and high temperatures. They were conducted on geopolymers having cure times of 28 days.  $H_2SO_4$  and  $HNO_3$  solutions as well as  $MgSO_4$  and  $Na_2SO_4$  solutions were used, leaving the geopolymeric specimens immersed for 7, 28 and 56 days. Compressive strength tests at high temperature were carried out at 200, 400, 600, 800 and 1000 °C for 2 h.

### 3. Results and discussion

#### 3.1 Mineralogy and geochemical properties of the raw materials

##### 3.1.1 Gold mining waste

Figure 1a illustrates the IR spectrum characteristic of the geological material (gold mining waste) used in the preparation of geopolymers. Each of the

crystalline phases identified is within the wavelength range of 500 to 3500  $cm^{-1}$ . The occurrence of sulfides and oxides in the IR spectrum is observed in the wavelength range of 300-1000  $cm^{-1}$  (Perez, 2008). On the other hand, quartz may be easily identified within the region between 1000 and 1500  $cm^{-1}$  (Rojas-López *et al.*, 2006). Muscovite can be identified in the wavelength range of 1400-2200  $cm^{-1}$ , although it shows a poor performance in the IR spectrum (Riaza *et al.*, 1994). The carbonates can be identified in a wide range of wavelengths (750-3500  $cm^{-1}$ ). According Riaza *et al.* (1994), their behavior resembles that of quartz and must always be greater than that of micas.

The qualitative analysis by X-ray diffraction (Figure 1b) of the gold mining waste reveals that this geomaterial consists of different crystalline phases (quartz, muscovite, pyrite, alunite and goethite). On the other hand, the quantitative analysis reveals in general terms, a compositional predominance of quartz (52.9 %), muscovite (12.9 %), pyrite (6 %), alunite (6.1 %) and goethite (4.1 %).

The chemical composition of the mining waste, which was determined by X-ray fluorescence, reveals a predominance of  $SiO_2$  (61.8%). It is well known that a geopolymerization process is successfully performed in the vast majority of materials in the presence of aluminosilicate compounds (Davidovits, 1994), and the  $SiO_2/Al_2O_3$  ratio is a parameter that influences not only the preparation of a geopolymer material but also its performance and durability (Duxson, 2006). The mining waste has a  $SiO_2/Al_2O_3$  ratio of 6.6, which is very high compared to the range of 3.0-3.8 proposed by Duxson *et al.* (2007) to perform successfully a geopolymerization process.

##### 3.1.2 Aggregate

The aggregate used in the preparation of geopolymers corresponds to a very coarse-grained (1.19 mm) arkosic sand size, which presents particles predominantly non-spherical sub-angular to sub-rounded, and is composed of quartz, feldspar and lithic fragments. Figure 2a illustrates the

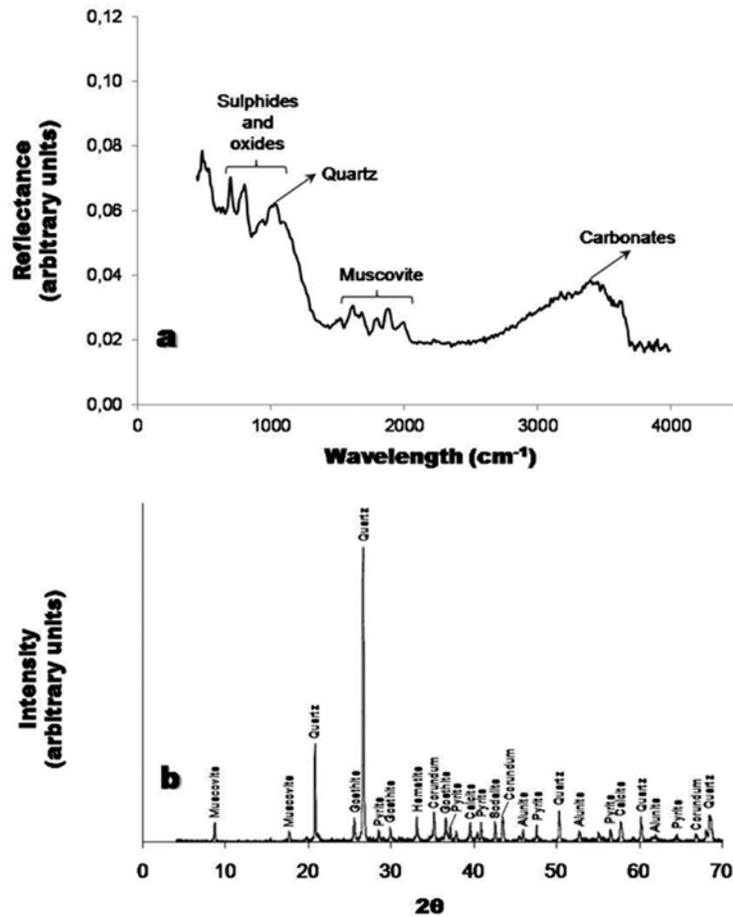


Figure 1. (a) IR spectrum and (b) X-ray diffraction pattern of the gold mining waste.

characteristic IR spectrum of the aggregate, which reveals different mineral phases within the range of wavelengths between 800 and 3800  $\text{cm}^{-1}$ . Taking into account the response of quartz ( $\lambda = 1000$  to  $1500 \text{ cm}^{-1}$  and high reflectances) and muscovite ( $\lambda = 1400$  to  $2200 \text{ cm}^{-1}$  and low reflectances) in the IR spectrum, it is proceeded to the identification of feldspars and lithic fragments. Although feldspars exhibit a behavior similar to that of quartz (Riaza *et al.*, 1994), it is possible to distinguish them, since the former will be within a shorter wavelength range ( $800\text{-}900 \text{ cm}^{-1}$ ). The rock fragments may be a special case due to their difficulty during identification. Riaza *et al.* (1994) consider that to identify any type of rock in the IR spectrum, it is necessary to emphasize particularly on the mineralogical composition of the sample. The heterogeneous nature of the lithic fragments in the aggregate, of

difficult determination, was resolved due to the atypical behavior observed in the wavelength of  $3800 \text{ cm}^{-1}$ , which is characteristic of lithic fragments. The apparent mineralogical homogeneity of the arkosic sand, was counter-argued with the qualitative and quantitative analysis by X-ray diffraction of the crystalline phases, which showed a group of minerals that could not be seen in the macroscopic description. The X-ray diffraction pattern (Figure 2b) shows the presence of clinocllore (6.3%), a typical mineral of some metamorphic rocks. This percentage would be associated with the high percentage content of lithic fragments found in the aggregate, taking into account that this is mainly constituted of relict igneous and metamorphic rocks. Quantitative analysis reveals the presence of albite type plagioclase (30.7%) and microcline type potassium feldspar (18.7%).

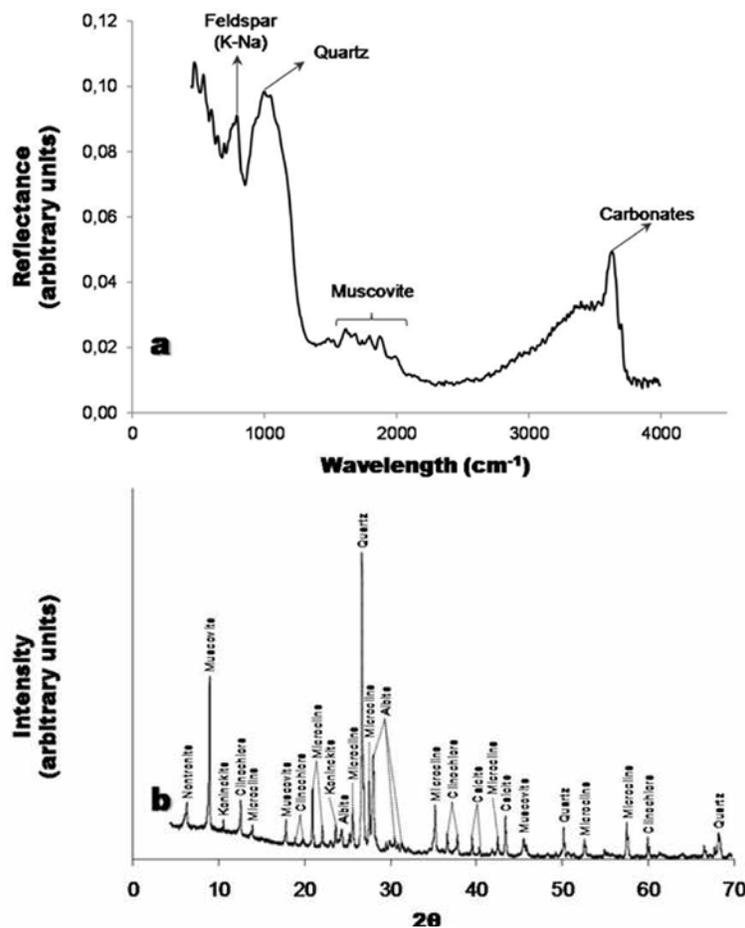


Figure 2. (a) IR spectrum and (b) X-ray diffraction pattern of the aggregate.

Results from X-ray fluorescence show that there is a pronounced predominance of aluminosilicate compounds ( $\text{SiO}_2$  68.0% and  $\text{Al}_2\text{O}_3$  18.6%, respectively). Given that the  $\text{SiO}_2/\text{Al}_2\text{O}_3$  ratio is 3.6, the probability of success during a geopolymerization reaction is one more time sustained as a chemical type constrain. This value is within the range of success in the geopolymerization reaction proposed by Duxson *et al.* (2007).

### 3.2 Compressive strength, performance and durability tests

#### 3.2.1 Compressive strength

The values of compressive strength at which the synthesized mortars were tested are summarized in Figure 3. There is a constraint of chemical type

that controls the performance of the geopolymers. It shows that when the concentration of the NaOH solution into the activating solution was increased, there is a better performance of the specimens in the compressive strength test. The specimens were always above the type I Portland cement are those in which the starting material was used as a substituent in 80% and 90%, which correspond to the geopolymers labeled as GEW-80-8/16 and GEW-90-8/16, respectively. This constraint had already been studied by Wang *et al.* (2005), checking if one increases the concentration of the components of the activating solution on average of 4 to 12 (n/L), the geopolymerization reaction would help to obtain higher compressive strength materials. Geopolymers synthesized using 50% (GEW-50-8/16) and 70% (GEW-70-8/16) of the starting

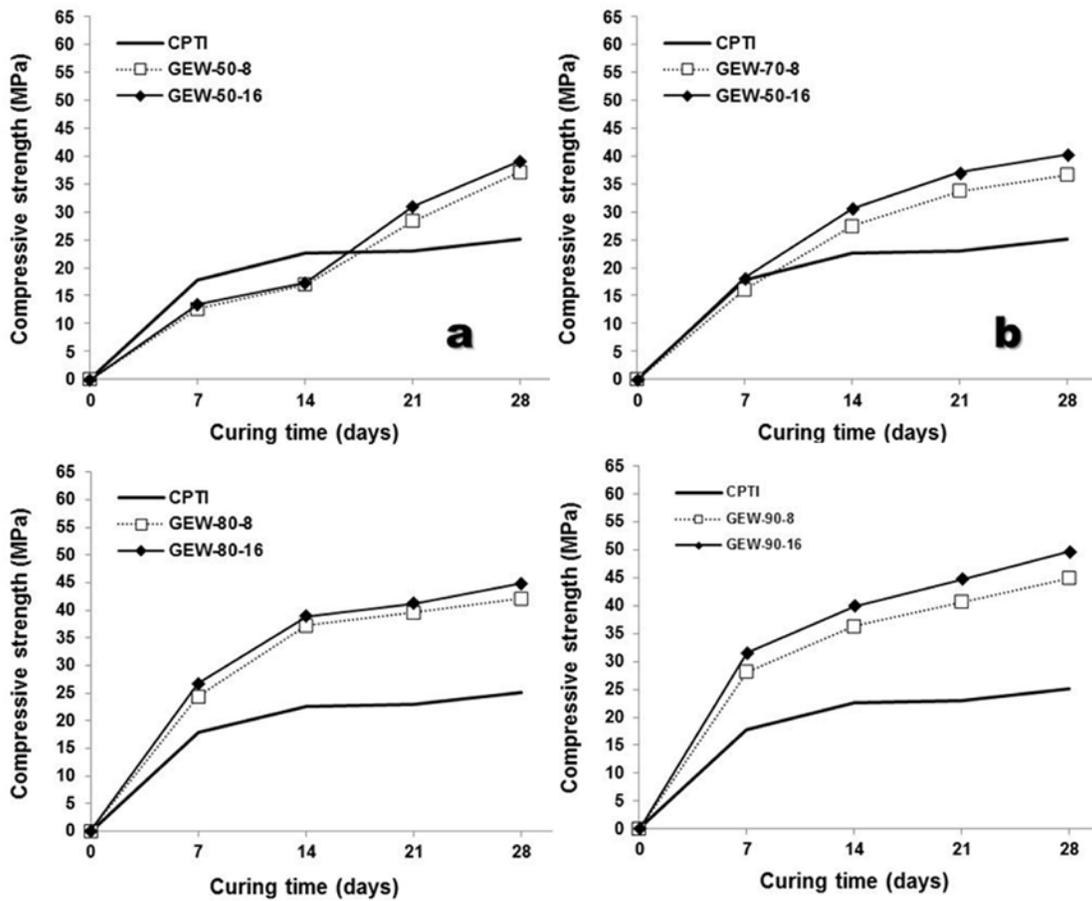


Figure 3. Compressive strength of mortars versus curing time.

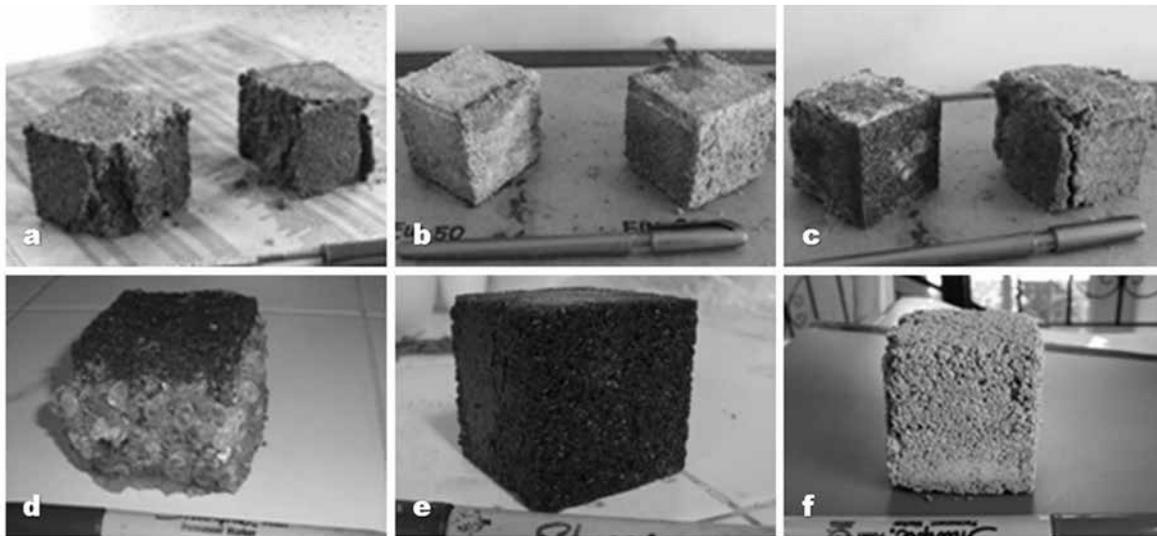
material show a lower performance in the early days of curing with regard to those made with whole percentage of type I Portland cement, and their behavior is much higher in the medium- and long-term for curing ages of 21 days for the first of them and 14 days for the second of them.

The most frequent phenomenon in these trials was the fracture of geopolymers in brittle conditions (Figure 4a). However, cases where the cohesion of the material remained almost entirely also presented. Taking into account that all geopolymers were synthesized at the same temperature and curing time (at 70 °C for 12 h), one of the main causes of this fact would have to do in the manner in which the specimens were placed in the testing machine. The maximum value of compressive strength reached for curing ages of 28 days. Therefore, this was the main experimental argument to evaluate

the performance and durability of geopolymers in other compressive strength tests (resistance to acids and sulfate attack, and resistance to high temperatures). In general, gold mining waste-based geopolymers show a greater compressive strength than that of type I Portland cement-based mortars.

### 3.2.2 Resistance to acid attack

Once defined that geopolymers with curing ages of 28 days would be subjected to several tests, it was decided to perform tests on the compressive resistance of materials after immersing in acidic solutions. The response of the specimens was uniquely different when two types of acids were used. Immersion times in these solutions were 7, 21 and 56 days. Results of these tests are summarized in Figure 5. It is noteworthy the negative effect of the HNO<sub>3</sub> acid solution, which



**Figure 4.** General trends on the mechanical strength, and performance and durability of geopolymers: (a) fragile fracture to compressive strength, after of attack with (b) sulfuric acid and (c) nitric acid, (d) crystallization of geopolymer in  $\text{Na}_2\text{SO}_4$  solution, (e) physical hardening of geopolymer after immersion in  $\text{MgSO}_4$  solution, (f) change in tone and cohesion of geopolymer at high temperatures.

was much greater than that of the  $\text{H}_2\text{SO}_4$  acid solution. Experimentation showed that during the first days of immersion in both solutions a phenomenon of saturation of the pore space of the geopolymer occurred. At this point, there was a significant change in the weight value of each of the specimens. This physical change produced a slight improvement in the strength of the material itself.

The value of the compressive strength of the specimen that has not been immersed in acid solutions is less compared to that obtained after completion of such immersion. Once more the constraint of chemical type plays an important role in the compressive resistance of materials. Those geopolymers were synthesized with an activating solution of  $\text{NaOH}$  (16M) and  $\text{Na}_2\text{SiO}_3$ , showed a better performance with regard to those activated in a solution of  $\text{NaOH}$  (8M) and  $\text{Na}_2\text{SiO}_3$ , as suggested by Wang *et al.* (2005), and which was proved in the rest of results obtained from the performance and durability tests of geopolymers. Although the effect in the short-term, using either of the two types of acids, it was favorable for the mechanical strength of geopolymers. It is

evident that there was an adverse effect in the medium- and long-term. For immersion times in acid solutions of 28 and 56 days, an apparent decrease in the ability of the geopolymer for resisting a compressive load was observed.

In all cases, the cohesion of the material was maintained when tested in sulfuric acid solutions (Figure 4b). A physical change was noted in the specimens as revealed by their dark green to yellowish brown color. This situation was reversed when the specimens were immersed in nitric acid solutions (Figure 4c). In this case, the material was almost entirely corroded after 56 days, undergoing a process of partial brittle fracture of structure.

### 3.2.3 Resistance to sulphate attack

As in the test of compressive resistance to acid attack, geopolymers of curing ages of 28 days were tested to simulate conditions typical of some coastal saline environments. Sulfate solutions of  $\text{MgSO}_4$  and  $\text{Na}_2\text{SO}_4$  and immersion times of 7, 21 and 56 days were also used. Results obtained were unique and different from each other. Figure 6 shows the performance of geopolymers

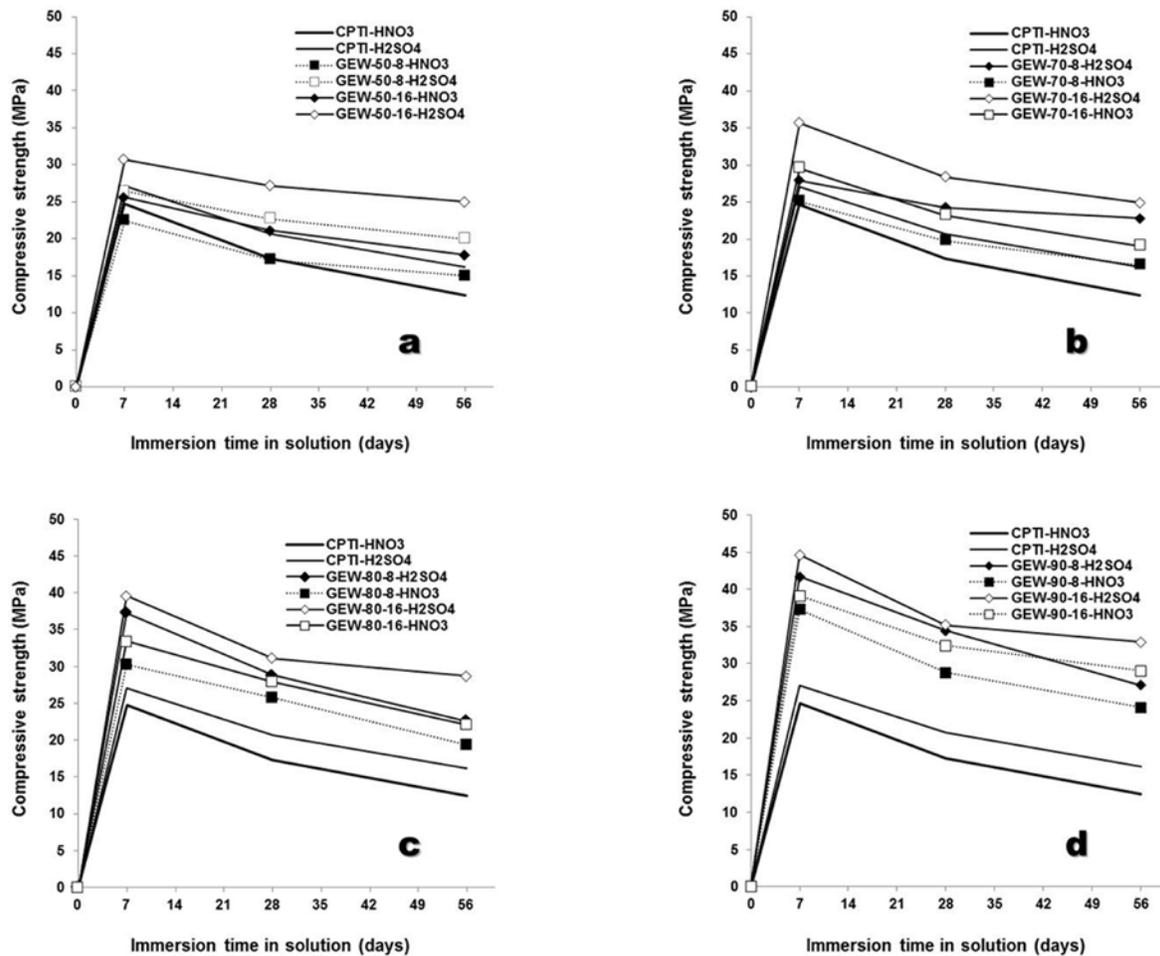


Figure 5. Compressive strength of mortars after acid attack.

after sulphate attack and reveals a completely different behavior that after acid attack. Contrary to what was expected, considering that we sought to generate an adverse environment for the performance and durability of geopolymers, the tests showed that the sulphate attack increased the mechanical properties of these materials. The general behavior for all tested mortars showed an enrichment of the indigenous capacity of inorganic cements to resist increasingly large compressive loads. In addition to the already proven constraint of chemical type on the favorability of the mechanical properties when an alkaline solution with a molar increase in one of its parts is used, we consider that the gold mining waste is an additive that can increase the durability of the conventional Portland cement in the medium- and long- term.

Unlike the behavior described for the mortars tested under acid attacks, and regardless of the gold mining waste/type I Portland cement ratio, the performance of geopolymer cements was always higher in each of the experimental periods of time. However, the physical changes caused by the specimens tested at the end of the trials were very different when a specific kind of sulphate used. When the performance and durability test was developed on geopolymers after immersion in a solution of Na<sub>2</sub>SO<sub>4</sub> at different periods of time, a phenomenon of crystallization of salt occurred (Figure 4d). It is very likely that this crystal growth around most of the specimens has positively affected their mechanical properties.

Proportionally to the phenomenon of salt crystallization of salt, there was a progressive

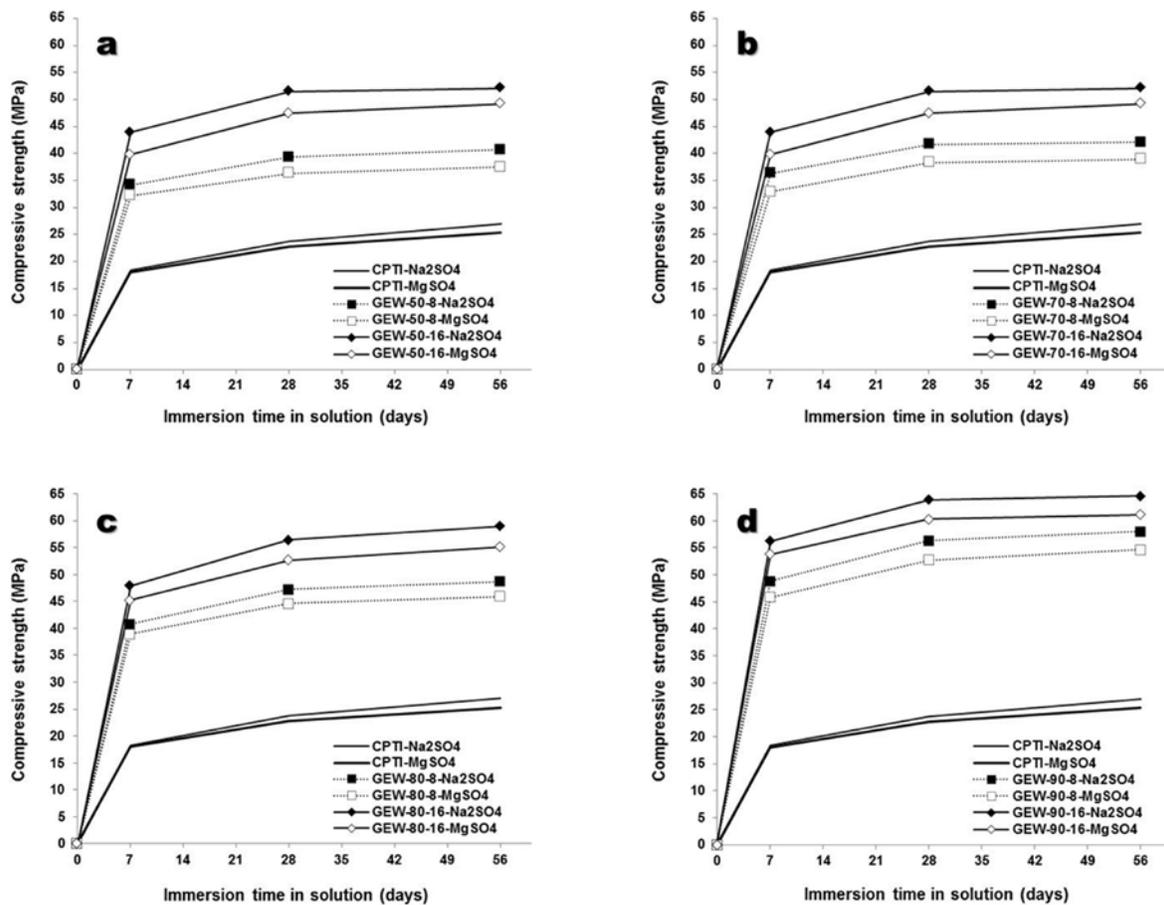


Figure 6. Compressive strength of mortars after sulphate attack.

increase in the weight of the geopolymer and the compressive strength. A higher increase on of the mechanical properties of the geopolymer was also observed when the solution of  $MgSO_4$  was used. Unlike the previous case, there was a phenomenon of crystallization of salt, but on the contrary, there was a complete hardening of the tested geopolymer (Figure 4e). At no time of experimentation brittle fracture phenomena were observed in the materials, another major difference between tests of resistance to acid attacks.

### 3.2.4 Resistance to high temperatures

Figure 7 illustrates the results of the tests of resistance to high temperatures, where an increasingly negative behavior (inversely proportional relationship). It was experimentally

determined that the greater the magnitude of the test temperature, the lower the mechanical strength of the material. Once more, the synthesized geopolymers with NaOH (16M) and  $Na_2SiO_3$  show the best performance and durability. As in the test of resistance to sulphate attack, all mortars manifest mechanical strength values that are well above those obtained for type I Portland cement-based mortars. The geopolymers with higher percentage of substitution (for example those geopolymers labeled as GEW-80-8/16 and GEW-90-8/16) produced higher mechanical strength. Significantly, this particular fact was already registered in the compressive strength tests, and in the tests of resistance to acid and sulphate attack.

The test of resistance to high temperatures is a completely destructive testing and besides the

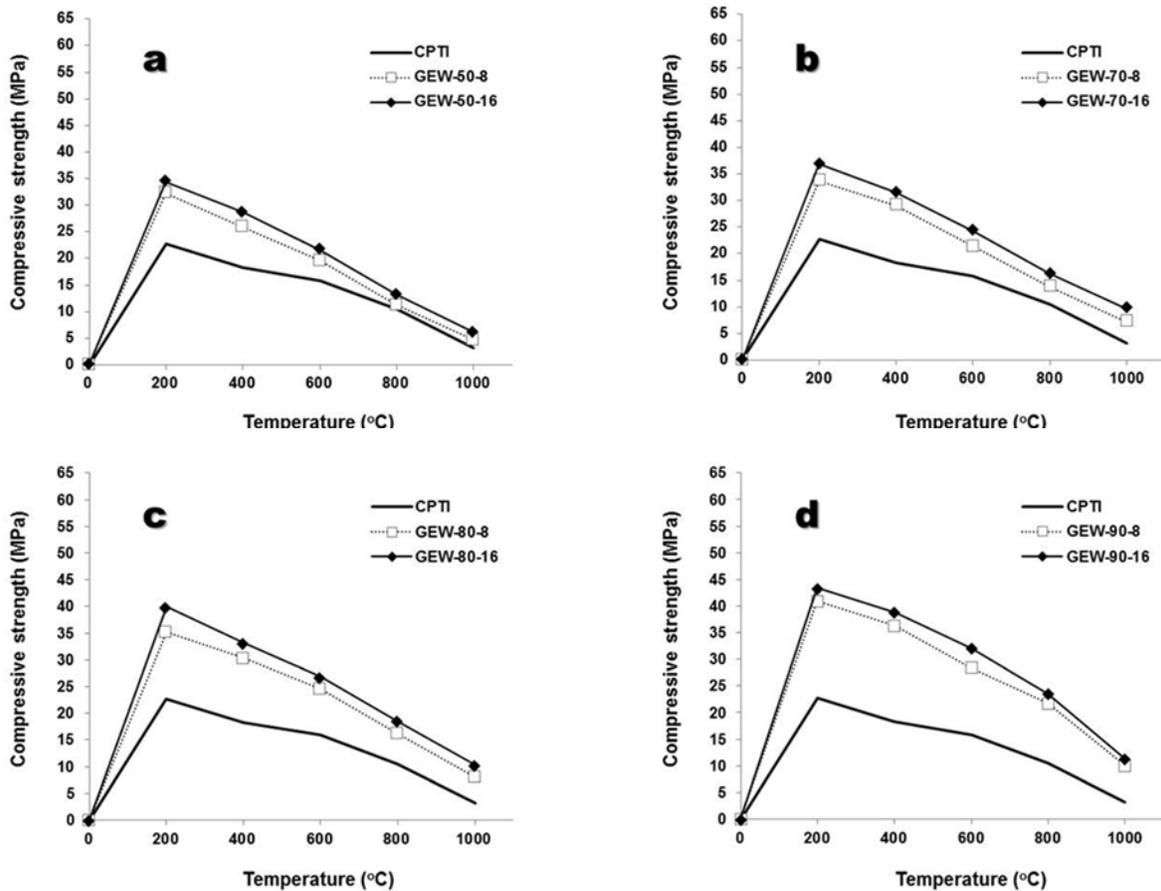


Figure 7. Compressive strength of mortars under high temperatures.

remarkable change in the color of test specimens (Figure 4f), brittle fracture phenomena were observed with temperature increasing.

Therefore, at least is demonstrated from the experimental point of view on a small scale that the geopolymeric cements have a higher response regarding to type I Portland cement, whatever the performance and durability test employed. While it is true that conventional cements are materials with high mechanical strength, it was seen that the gold mining waste-based geopolymers are above these routine materials and can be considered as alternative materials with high performance and durability over time.

#### 4. Conclusions

Results show that gold mining wastes are suitable in the preparation of geopolymeric

products, which are environmental friendly, low production cost, high compressive strength, and excellent performance and long-term durability. This work not only enabling the production of new geopolymers but also contributes to the solution of the environmental concern by mining waste disposal. The compressive strength test reveal that geopolymers prepared from alkali activation of gold mining waste show compressive strength values above those obtained in the commercial Portland cement. Geopolymers prepared from nearly complete replacement of type I Portland cement and cured at 70 °C for 12 h, shows the higher values of compressive strength. Therefore, these results reveal a real possibility of using gold mining waste-based geopolymers as alternative materials to the type I Portland cement.

## 5. Acknowledgements

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